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# To the theory of underwater ice evolution, or nonlinear dynamics of "false bottoms"

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#### 1. Introduction

During the summer, when the air temperature is above 0 °C the sea ice - atmosphere interface undergoes ablation to occur. A considerable fraction of meltwater gathers in surface puddles thereby reducing the surface albedo. This meltwater can percolate into the ice matrix, leading to a strong reduction in the surface salinities. Untersteiner [1] showed that the meltwater flux into the ice reduces salinities at the top of the ice column to values close to zero. As a result of these processes, low-salinity meltwater comes into contact with seawater, each at or close to their respective freezing points. This meltwater can be retained under thin ice in bottom depressions, leading to fresh water lenses or forming what Hanson calls "under-ice melt ponds" [2]. Martin and Kauffman demonstrated in their laboratory experiments that freezing of under-ice melt ponds can be explained by double-diffusion at the interface between freshwater and seawater [3]. Initially, ice platelet crystals would form in the contact zone and grow to centimeter or decimeter size if an attachment prevented their removal from the halocline. Subsequently, more solid ice cover would form along the entire freshwater - seawater interface, stabilized by a mesh of crystals and other anchor processes. This underwater ice is called false bottoms [2–6]. When this underwater ice sheet forms, it migrates upwards due to bottom ablation [2,3] (for example, the Arctic Ice Dynamics Joint Experiment (AIDJEX) demonstrated some rapid upward migration of the false bottoms with relation to ablation under nearby thick ice). The field experiment Surface Heat Budget of the Arctic Ocean (SHEBA) showed that approximately

#### ABSTRACT

We present a mathematical model describing evolution of false bottoms often met between an under-ice melt pond and the underlying ocean during summer. The model treats a false bottom as the region of mixed phase (mushy layer) whose coordinates depend on time and determine the phase transition area. As the heat and the salt fluxes in the ocean are strongly influenced by turbulence and the ice meltwater accumulating underneath the ice cover is practically fresh, we use modified boundary conditions for heat and mass fluxes at the interfaces of phase transition. Explicit analytical solutions (thickness of false bottom and growth rates of its boundaries, temperature and salinity distributions, solid phase fraction and ocean-to-ice heat flux) of the nonlinear model under consideration are found. Model predictions are in good agreement with existing experimental data and physical concepts of phenomena under study.

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15% of a total of more than 100 mass-balance gauges developed false bottoms during the ablation season [6,7]. It has been found experimentally that under-floe melt ponds and false bottoms covered half of the flow bottom of the drifting station "Charlie" [2]. It is important to keep in mind that the formation of false bottoms is the only process by which significant amounts of new ice can be formed during the summertime. Nansen from his observations in the Beaufort Sea noted that the heat transfer from the trapped fresh water, with a temperature of 0 °C, to the arctic sea water, with a temperature of -1.6 °C, is the only source of ice accretion during the polar summer [8]. An additional point to emphasize is that false bottoms play an important role as reservoirs of meteoric water (snow meltwater). They are important in the transfer of pollutants from the atmosphere into the ice pack [9]. Taking into account all things considered, we present a theory of false bottom migration on the basis of macroscopic heat and mass transfer equations and boundary conditions when the phase transition occurs in a mixed layer (mushy region) and the heat and mass fluxes in the ocean are influenced by turbulence.

### 2. Model of false bottom evolution

Let us now consider the process when a false bottom directionally freezes upwards. We describe a system once a thin veneer of young ice representing a false bottom has been formed (the initial formation of false bottoms usually took only a couple of hours in natural conditions [10]). A schematic diagram of the process is plotted in Fig. 1 (here *z* is the spatial coordinate, a(t) and b(t) are the fresh water – false bottom and false bottom – sea water phase transition interfaces, respectively, *t* is the time). The regions a(t) < z < 0, z < b(t) and b(t) < z < a(t) are, respectively, filled

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Nomenclature			
а	fresh water – false bottom boundary	и	friction velocity
b	false bottom – sea water boundary	Z	spatial coordinate
Cw	specific heat of water		
D	molecular diffusivity of salt in sea water	Greek symbols	
$k_{\rm i}$	thermal conductivity of ice	α <sub>h</sub>	turbulent coefficient for heat
kw	thermal conductivity of water	α <sub>s</sub>	turbulent coefficient for salt
$L_V$	latent heat	$\rho_{w}$	density of water
т	liquidus slope	$\varphi$	solid phase fraction
Sm	salinity		
$S_{\infty}$	salinity far from phase transition boundaries in the	Subscrip	ts
	ocean	$a$ and $\hat{b}$	point at the physical parameters of boundaries of
t	time		$\hat{b}(t)$ .
$T_{\infty}$	temperature far from phase transition boundaries in the		
	ocean		

with the fresh water, the sea water and the false bottom consisting of a mixed (liquid and solid phases) zone [3,5]. We shall treat this zone as a quasi-equilibrium mushy layer [11,12]. Since a relaxation time of the temperature field is far less than characteristic times of the process, the temperature field in the mushy layer (false bottom) will be considered as a linear function of the spatial coordinate

$$T_m(z,t) = \frac{T_a(t)(z - b(t)) + T_b(t)(a(t) - z)}{a(t) - b(t)}, \quad b(t) < z < a(t),$$
(1)

where  $T_a$  and  $T_b$  stand for the temperatures at the phase transition boundaries *a* and *b*. The linear form (1) of the temperature field is confirmed by laboratory experiments [3]. Physically this means that the temperature field and the solid fraction  $\varphi(z, t)$  within the false bottom undergo only insignificant oscillations with time ( $\varphi$  is also with z). Theoretically this conclusion was demonstrated by Alexandrov and Malygin [13] and by Alexandrov et al. [14] for solidification of leads. Taking into account that the salinity field  $(S_m(z,t))$ 



Fig. 1. (a) A sketch of an under-ice melt pond [3]. (b) A schematic diagram of the process.

a(t) and

in the mush is a nearly linear function of z (see among others, [3]), we use the Scheil formula [15]

$$\frac{\partial}{\partial t}((1-\varphi)S_m) = 0, \quad b(t) < z < a(t).$$
(2)

Eq. (2) implies that all salt is displaced by ice into the liquid matrix of the system. We shall consider that the mushy layer (false bottom) is in thermodynamic equilibrium. Therefore, the temperature and salinity distributions are related by the liquidus equation

$$T_m(z,t) = -mS_m(z,t), \quad b(t) < z < a(t),$$
 (3)

where *m* is the liquidus slope. The linear form of Eqs. (1) and (3)agrees closely with the laboratory experiments [3] where nearly linear functions  $T_m$  and  $S_m$  with respect of z have been observed.

Laboratory experiments [3] show that heat and the salt fluxes at the phase transition boundary z = a(t) determined from the fresh water side are far less than their analogs determined from the mushy layer side. This being the case, the heat and mass balance boundary conditions can be written in the form

$$L_V \varphi_a \frac{\mathrm{d}a}{\mathrm{d}t} = (k_i \varphi_a + k_w (1 - \varphi_a)) \frac{\partial T_m}{\partial z},\tag{4}$$

$$S_a \frac{\mathrm{d}a}{\mathrm{d}t} = -D \frac{\partial S_m}{\partial z},\tag{5}$$

where  $L_V$  is the latent heat parameter, D is the diffusion coefficient, k is the thermal conductivity, the subscripts i and w refer to ice and water, respectively. Eq. (5) indicates that the rate of salt diffusion must be sufficient to keep up with the rate of boundary a(t) (this model assumption is backed by the laboratory experiments [3] demonstrating that the salinity gradient is practically negligible in the fresh water region at  $z \ge a(t)$ ).

As the rate of motion of the phase transition boundary z = b(t)undoubtedly depends on the turbulent motion in the ocean, let us write down the boundary conditions as follows [10,16,17]

$$L_V \varphi_b \frac{db}{dt} = (k_i \varphi_b + k_w (1 - \varphi_b)) \frac{\partial T_m}{\partial z} + \alpha_h \rho_w c_w u (T_\infty - T_b), \tag{6}$$

$$S_b \varphi_b \frac{\mathrm{d}b}{\mathrm{d}t} = \alpha_s u (S_\infty - S_b),\tag{7}$$

where  $T_{\infty}$  and  $S_{\infty}$  are the far-field properties of the salt water, *u* is the friction velocity,  $\rho_w$  and  $c_w$  are the density and the specific heat of water,  $\alpha_h$  and  $\alpha_s$  are the turbulent transfer coefficients for heat and salt respectively. The ratio of exchange coefficients  $\alpha_h/\alpha_s$ depends on the molecular diffusivities for heat  $(\kappa)$  and salt (D) at that  $\alpha_h/\alpha_s = (\kappa/D)^n$  [17] with 2/3 < n < 4/5 [18,19]. We put  $35 \leqslant \alpha_h/\alpha_s \leqslant 70$  after Notz et al. [10]. The aforementioned model (1)-(7) represents a nonlinear set of equations and boundary conditions imposed at moving phase transition interfaces. This model describes nonstationary freezing in the presence of a mushy layer, playing the role of a false bottom, with heat and salt fluxes at the lower boundary influenced by turbulence. How to construct exact analytical solutions of the above-mentioned model is discussed below.

#### 3. Exact analytical solutions

Integrating Eq. (2), we find the solid phase fraction in the mushy layer

$$\varphi(z,t) = 1 - \frac{(1 - \varphi_b)T_b}{T_m(z,t)},$$
(8)

where  $T_m(z,t)$  is determined by expression (1). Combining the boundary conditions (4), (5) and taking into account Eq. (3), we get the solid phase fraction at the upper phase transition interface

$$\varphi_a(t) = \frac{KT_a(t)}{(K-1)T_a(t) - T_p}, \quad K = \frac{k_w}{k_i}, \quad T_p = \frac{DL_V}{k_i}.$$
(9)

Now substituting  $\varphi_a(t)$  from expression (9) into expression (8) at z = a(t), we obtain temperature  $T_b$  at the lower boundary in terms of temperature  $T_a$  at the upper boundary

$$T_b(T_a(t)) = \frac{T_a^2(t) + T_a(t)T_p}{(\varphi_b - 1)((K - 1)T_a(t) - T_p)}.$$
(10)

As the temperature and salinity fluxes are proportional in accordance with Eqs. (1) and (3) we can find a set of equations connecting the mushy layer (false bottom) thickness h(t) = a(t) - b(t) and the phase transition temperature  $T_a(t)$ . With this aim in mind we equate derivatives db/dt from Eqs. (6) and (7) and subtract derivatives in the left-hand sides of Eqs. (4) and (7). As a result, we have

$$a(t) - b(t) = Q_1(T_a(t), t),$$
 (11)

$$\frac{d(a(t) - b(t))}{dt} = \frac{Q_2(T_a(t))}{a - b} + Q_3(T_a(t), t),$$
(12)

where

$$\begin{split} Q_1(T_a(t),t) &= -\frac{(k_i\varphi_b + k_w(1-\varphi_b))(T_a - T_b)T_b}{\alpha_s u L_V(T_b + mS_\infty) + \alpha_h \rho_w c_w u(T_\infty - T_b)T_b},\\ Q_2(T_a(t)) &= \frac{(k_i\varphi_a + k_w(1-\varphi_a))(T_a - T_b)}{L_V\varphi_a},\\ Q_3(T_a(t),t) &= \frac{\alpha_s u(T_b + mS_\infty)}{T_b\varphi_b}. \end{split}$$

Here we bear in mind that the arguments of functions  $Q_1, Q_2$  and  $Q_3$  may be dependent on time in an explicit form (not only by means of dependence  $T_a(t)$ ) in the case that  $u, T_\infty$  or  $S_\infty$  are time-dependent too.

Let us now consider the special case that all values  $u, T_{\infty}$  and  $S_{\infty}$  are constants (or all of them are averaged over their variations in time and changed by constants). Then  $Q_1$  and  $Q_3$  as well as  $Q_2$  depend on t only as composed functions of  $T_a(t)$ . If this is really the case, substitution a(t) - b(t) from (11) into (12) gives an explicit function  $t(T_a)$  of the form

$$t(T_a) = \int_{T_{a0}}^{T_a} F(T_a) dT_a, \quad F(T_a)$$
  
=  $\frac{dQ_1(T_a)}{dT_a} \frac{Q_1(T_a)}{Q_2(T_a) + Q_1(T_a)Q_3(T_a)}.$  (13)

The initial temperature  $T_{a0}$  (determined at t = 0) can be found from the algebraic Eq. (11) on condition that the initial coordinates a(0)and b(0) are known. Once integral in the right-hand side of (13) has been calculated, the inverse function  $T_a(t)$  can readily be obtained.

In the general case when one of the values  $u, T_{\infty}$  or  $S_{\infty}$  becomes dependent on time, we can get the initial-value problem (Cauchy

problem) for  $T_a(t)$ ; if so, substitution a(t) - b(t) from (11) into (12) gives

$$\frac{dT_a(t)}{dt} = f(T_a, t), \quad T_a(0) = T_{a0},$$
(14)

where  $f(T_a, t)$  is known function. For the sake of simplicity, we will not write out this elementary but exceedingly lengthy dependence. The initial point  $T_{a0}$  is determined, as before, by Eq. (11).

We are now in position to describe the laws of motion of boundaries a(t) and b(t); to accomplish this, let us integrate expression (7) and arrive at the law for lower boundary

$$b(t) = b(0) - \int_0^t \frac{\alpha_s u(T_b(T_a) + mS_\infty)}{T_b(T_a)\varphi_b} dt,$$
(15)

where  $T_b(T_a)$  and  $T_a(t)$  are determined by expressions (10), (13) or (14). The law of upper boundary follows from Eq. (11) and has the form

$$a(t) = b(t) + Q_1(T_a(t), t).$$
 (16)

#### 4. Model predictions for field experiments

Let us now compare model predictions and experimental data on false bottom evolution taken from the AIDJEX and the SHEBA field experiments (see, among others, [20,21]). Since the solid fraction  $\varphi_b$  is in close proximity to unity, we choose  $\varphi_b = 0.99$ . Fig. 2 demonstrates the bottom elevation change during AIDJEX calculated on the basis of expression (15) for different friction velocities  $(b_1(t) = b(t) - b(0))$  and Fig. 3 shows time oscillations of the solid fraction  $\varphi_a$  and the heat flux  $J = \alpha_h \rho_w c_w u (T_\infty - T_b)$  that goes from the false bottom - ocean interface to the ocean (this direction corresponds to negative values of *I*). The far-field temperature,  $T_{\infty}$ , and salinity,  $S_{\infty}$ , as well as the friction velocity, *u*, can vary with time in natural conditions. Figs. 4 and 5 demonstrate such variations measured during the 1998 SHEBA campaign in accordance with ref. [10]. Using these experimental data as the base let us take a brief look at time-to-time variation of the false bottom thickness h(t) = a(t) - b(t). Fig. 5 demonstrates this function calculated on the basis of expressions (14)–(16). It is readily seen that the essentially increasing function h(t) becomes decreasing after day 207. The reason is that the storm came through, which substantially increased function u(t) (see Fig. 5 and Ref. [10]). As a result, the salt flux from the ocean to the ice increases, and in its turn a rapid ablation of the false bottom occurs. An increase of the brine salinity reduces the phase transition temperature  $T_b = -mS_b$  which becomes less than the ocean temperature  $T_{\infty}$ . By this is meant that the tem-



**Fig. 2.** Friction velocity during AIDJEX in accordance with Rossby-number similarity theory [10] (axis to the left). Experimental data in accordance with the AIDJEX field campaign and theoretical predictions (axis to the right). Two curves based on fixed values of *u* are calculated from expression (13) and one curve based on time oscillations of *u*(*t*) is calculated from expression (14). Thermophysical parameters used in calculations [3,10]:  $\alpha_{\rm h} = 0.0095, \alpha_{\rm h}/\alpha_{\rm s} = 35, k_{\rm w} = 5.86 \cdot 10^{-3}$  J/ (cm c °C),  $k_{\rm i} = 22.19 \cdot 10^{-3}$  J/(cm c °C),  $c_{\rm w} = 4.187$  J/(g °C),  $\rho_{\rm w} = 1$  g/cm<sup>3</sup>,  $L_{\rm V} = 308.16$  J/ (cm  $^{\circ}$  0,  $b_{\rm O} = 2.5$  cm,  $T_{\infty} = -1.5$  °C,  $m = 5.3 \cdot 10^{-2}$  °C psu<sup>-1</sup>,  $S_{\infty} = 29.8$  psu.



**Fig. 3.** The solid fraction at the fresh water – false bottom interface and the heat flux at the sea water – false bottom interface as the functions of time. These dependences are plotted in accordance with function u(t) shown in Fig. 2.



Fig. 4. Far-field temperature and salinity from SHEBA data.



**Fig. 5.** Friction velocity from SHEBA data and calculated evolution of the thickness of a false bottom (mushy layer), a(0) - b(0) = 1 cm.

perature difference  $\Delta T = T_{\infty} - T_b$  becomes negative and the heat flux *J* changes its sign. In other words, the ocean-ice heat flux in this case is directed toward the ice. Such a behavior is demonstrated to the second s



Fig. 6. Salinity and temperature oscillations predicted on the basis of our theory and SHEBA data.



Fig. 7.  $\Delta T$  and heat flux oscillations predicted on the basis of our theory and SHEBA data.



**Fig. 8.** Current and average heat transfer coefficients (Stanton numbers) calculated on the basis of AIDJEX (in the case of u(t)) and SHEBA data. Horizontal lines show corresponding average values,  $\langle St \rangle = 0.0067$  for AIDJEX and  $\langle St \rangle = 0.0047$  for SHEBA data.

strated in Figs. 6 and 7 where all functions are shown in accordance with the theory under consideration.

We now turn our attention to the question of current fluctuations in a Stanton number

$$\mathrm{St} = -lpha_\mathrm{h} rac{T_\infty - T_b}{T_\infty + mS_\infty}$$

shown in Fig. 8. A common way of treating ocean heat flux in theoretical and numerical models is to express the heat flux in terms of the heat exchange coefficient (Stanton number), relating the aggregate scale heat flux to ice interface friction velocity and elevation of mixed layer temperature above freezing [10]. Results from several studies have shown the Stanton number to be relatively uniform [22]. Its average values  $\langle St \rangle$  close to 0.0055 used in Ref. [10] for finding the turbulent transfer coefficients.

#### 5. Concluding remarks

In this paper, we have focused attention on the mathematical model of false bottoms that play an important role in the energy balance of Arctic sea ice. They frequently form at the interface between fresh and salt water bordering under-ice concavities in summer. During periods of the thickening of false bottoms there is a significant heat flux into the mixed layer of order  $10 \text{ W/m}^2$  [10]. For example, the model under consideration predicts that the ice-ocean heat flux can be directed upward or downward at different times, with an average value of  $-12.9 \text{ W/m}^2$  for AIDJEX and  $-5.6 \text{ W/m}^2$  for SHEBA data (the reason of upward direction is connected with abrupt jumps of the friction velocity). This flux is comparable to other heat flux from depth. Taking into consideration that under-ice melt pond formation might be a widespread phenomenon in the Arctic [23], an important role of model predictions

becomes clear to learn more about nonlinear dynamics of the Arctic Seas.

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